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## LETTER TO THE EDITOR

# Approximations for the fields under steady space-charge perturbed current flow 

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#### Abstract

Working approximations are given for the fields at the electrodes of a film sample in terms of the ratio between the steady excess current and its space charge limit.


One sometimes requires to determine the field distribution in a thin film sample carrying a steady, space-charge perturbed, excess current. For example, one might wish to deduce the field at the injecting electrode when the measured current density is $J$ and the spacecharge limit $J_{\text {SCL }}$ can be estimated. The field distribution is given by a well known expression (Mott and Gurney 1940, Lampert and Mark 1970) which, for our purpose, is best written as

$$
\begin{equation*}
F(\xi)=\frac{3}{2} \breve{F} f\left(\xi+\xi_{0}\right)^{1 / 2} . \tag{1}
\end{equation*}
$$

Here $\xi=x / L, x$ being the distance from the injecting electrode and $L$ the film thickness; $\xi_{0}$ is a constant of integration; $\bar{F}$ is the average field $V / L$ where $V$ is the applied voltage; and $f=\left(J / J_{\mathrm{SCL}}\right)^{1 / 2}$ where $J_{\mathrm{SCL}}=\frac{9}{8} \varepsilon \mu^{*} F^{2} / \mathrm{L}$ and $\mu^{*}$ represents the (generally) trapcontrolled effective carrier mobility, assumed to be independent of field. In particular, the fields at the injecting and counter electrodes are

$$
\begin{equation*}
F_{0}=\frac{3}{2} \bar{F} f \xi_{0}^{1 / 2} \quad F_{L}=\frac{3}{2} \bar{F} f\left(1+\xi_{0}\right)^{1 / 2} . \tag{2}
\end{equation*}
$$

The constant $\xi_{0}$ must be determined from the condition $\int F L \mathrm{~d} \xi=V$ which simplifies to

$$
\begin{equation*}
\left(1+\xi_{0}\right)^{3 / 2}-\xi_{0}^{3 / 2}=f^{-1} \tag{3}
\end{equation*}
$$

For a given value of $f, \xi_{0}$ must be found by computation. The author is not aware of any simple approximate solution for $\xi_{0}$ in terms of $f$ available in the literature, and the purpose of this letter is to offer such a working approximation.

Let $y=\frac{2}{3}\left(F_{L} / \bar{F}\right) f^{-1}$, then (2) and (3) yield

$$
\begin{equation*}
y^{3}-\left(y^{2}-1\right)^{3 / 2}=f^{-1} . \tag{4}
\end{equation*}
$$

For small enough $f$, expansion gives

$$
\begin{equation*}
y^{2}-\frac{2}{3} f^{-1} y-\frac{1}{4}=0 \tag{5}
\end{equation*}
$$

which has the approximate solution, linear in $f^{2}=J / J_{\text {SCL }}$,

$$
\begin{equation*}
F_{L} / \bar{F} \simeq 1+\frac{9}{16} f^{2} . \tag{6}
\end{equation*}
$$

For $J / J_{\text {SCL }} \leqslant 0.3$, this approximation differs from the computed values by $<1 \%$, but it

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Figure 1. $F_{L} / \bar{F}$ and $F_{0} / \bar{F}$ as functions of $J / J_{\mathrm{sCl}}$. Curves: computed; points: calculated from approximations (7) and (9).
clearly fails for larger arguments, since $F_{L} / \bar{F}$ should tend to 1.5 as $J$ approaches $J_{\text {SCL }}$. However, the ad hoc approximation, also linear in $J / J_{\mathrm{SCL}}$,

$$
\begin{equation*}
F_{L} / \bar{F} \simeq 1+0.5 f^{2}=1+0.5 J / J_{\mathrm{SCL}} \tag{7}
\end{equation*}
$$

turns out to be surprisingly good. The error is greatest, but only about $-1 \%$, for $J / J_{\text {SCL }}=0.3$, and tends to zero as $J / J_{\text {SCL }}$ approaches 0 or 1 . From (7) and (2) we then obtain

$$
\begin{equation*}
\xi_{0} \simeq \frac{1}{9}\left[4\left(J_{\mathrm{SCL}} / J\right)+\left(J / J_{\mathrm{SCL}}\right)-5\right] \tag{8}
\end{equation*}
$$

and

$$
\begin{equation*}
F_{0} / \bar{F} \approx\left[1-1.25\left(J / J_{\mathrm{SCL}}\right)+0.25\left(J / J_{\mathrm{SCL}}\right)^{2}\right]^{1 / 2} \tag{9}
\end{equation*}
$$

The errors in $\xi_{0}$ and $F / \bar{F}$ amount to about $-7.5 \%$ and $-4 \%$ respectively for $J / J_{\mathrm{SCL}}$ between 0.7 and 0.9 , but decrease towards zero as $J / J_{\text {SCL }}$ approaches 0 or 1 .

The curves in figure 1 show the computed dependence of $F_{L} / \bar{F}$ and $F_{0} / \bar{F}$ on $J / J_{\text {SCL }}$. The points represent values calculated from the approximations (7) and (9), which would seem to afford sufficient accuracy for most practical purposes.

## References


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